

Investigation of Structural Uncertainty of Wind Turbine Rotor Blades

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ForWind 
Center for Wind Energy Research Bremen
Hannover
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**Investigation of
Structural
Uncertainty of
Wind Turbine Rotor
Blades**

Outline

Introduction

Structural
Uncertainty

Simulation Process

Results

Conclusions and
Outlook

Outline

- 1. Introduction**
- 2. Modelling Structural Uncertainty**
- 3. Simulation Process**
- 4. Results**
- 5. Conclusions and Outlook**



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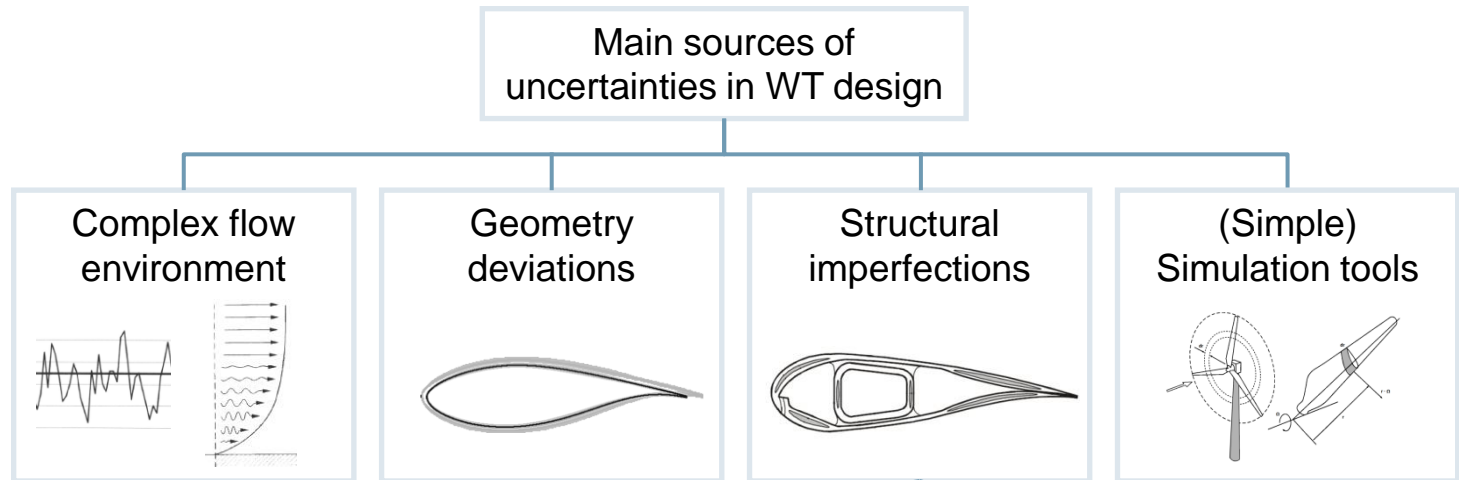
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Motivation

For long and slender rotor blades, the consideration of uncertainties and aeroelastic phenomena becomes increasingly important.



- Imperfections of composite materials due to the variability of
 - the fiber and matrix material properties,
 - fiber volume ratio,
 - ...
- Manufacturing tolerances due to non-automated processes



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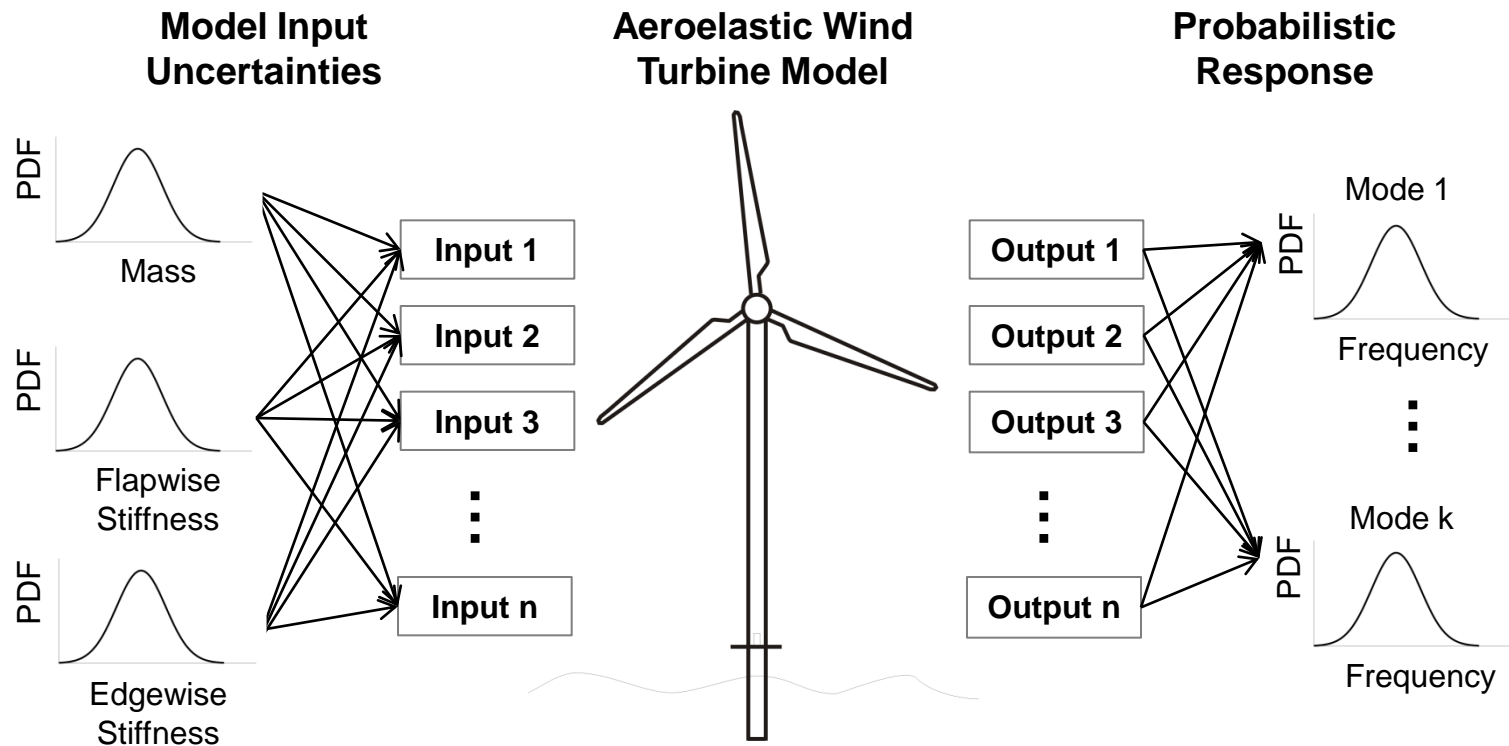
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Approach

Using spatial random fields and Latin hypercube sampling to investigate the effect of structural uncertainty of rotor blades on...

- 1) the full system mode shapes and
- 2) the system natural frequencies of an offshore wind turbine (OWT).





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Aeroelastic Wind Turbine Model

The aeroelastic model of the NREL 5MW reference wind turbine is used with 15 degrees of freedom (DOF).

- Pitch-controlled variable-speed wind turbine
- Based on available information of the REpower 5M and the DOWEC design study

Rated power	5000 kW
Rotor diameter	126 m
Hub height	90 m
Cut-in, rated, cut-out wind speed	3, 11.4, 25 m/s
Cut-in, rated rotor speed	6.9, 12.1 rpm

- Known data of:
 - blade structural and aerodynamic properties
 - nacelle and hub
 - drivetrain
 - tower
 - control system



Source: REpower



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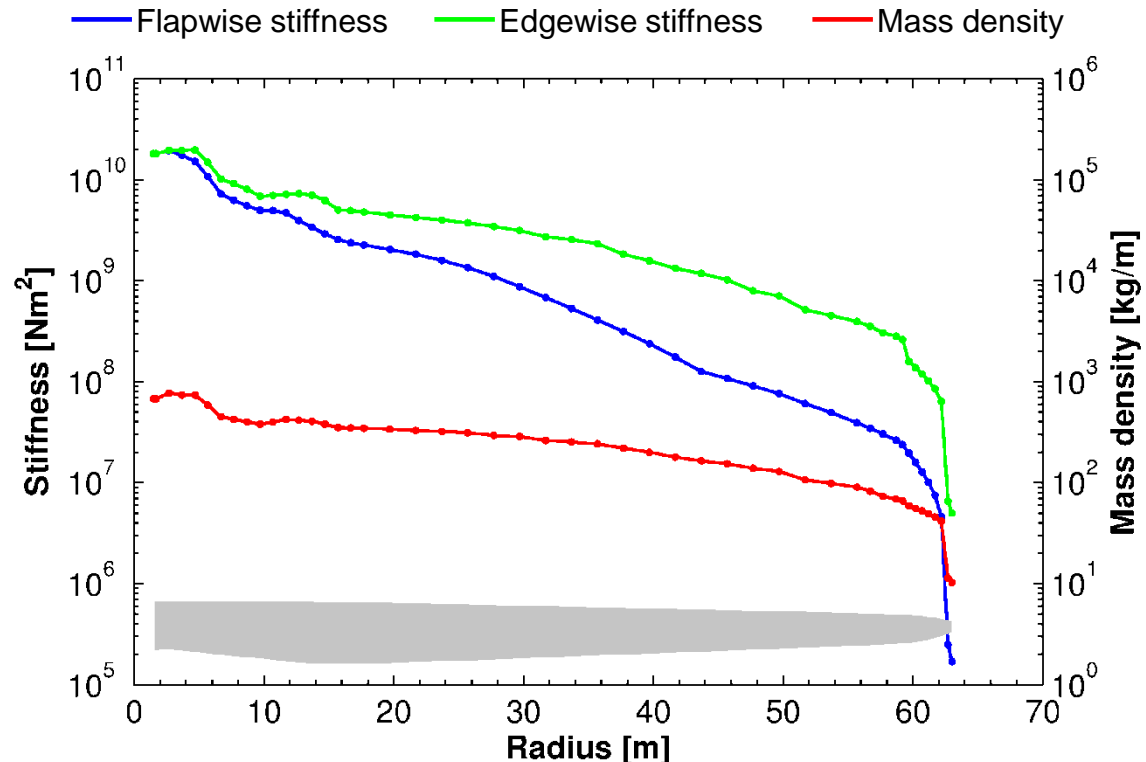
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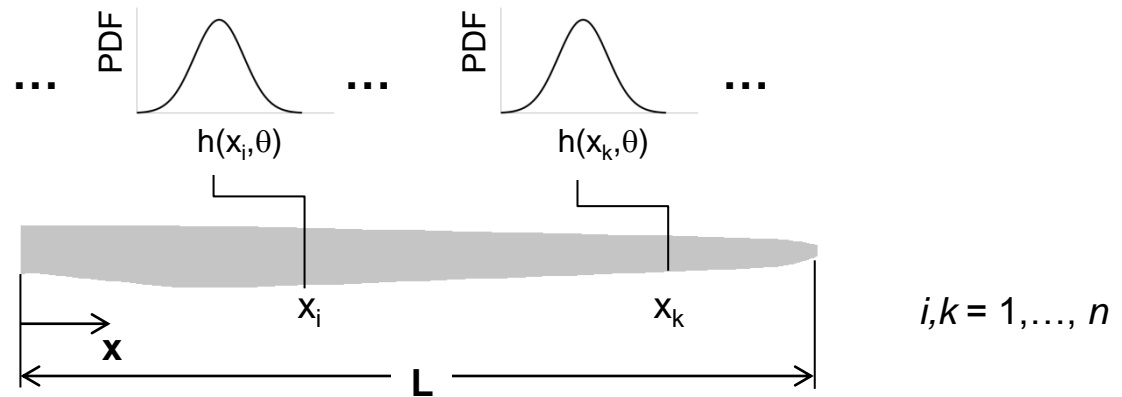
Modeling Structural Uncertainty of Rotor Blades



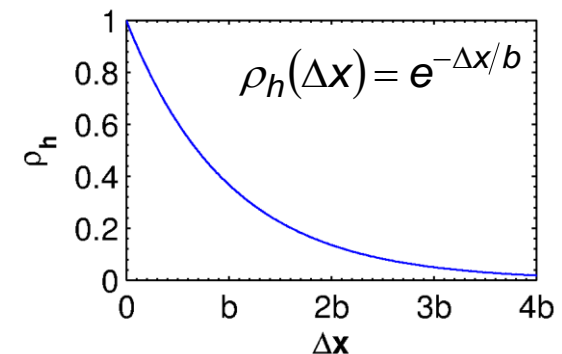
- Structural blade parameters are varied with respect to the corresponding baseline parameters.
- Variations are normally distributed ($\mu = 0\%$, $\sigma = 10\%$).
- Spatial variations of the structural parameters along the blade are...
 - uniform,
 - independent, or
 - correlated.

Homogeneous, Isotropic, Gaussian Random Field

Variations of structural properties, which are spatially correlated, can be described by a random field $h(x, \theta)$.



$$C_{hh} = \sigma^2 \cdot \begin{bmatrix} \rho_h(x_1, x_1) & \rho_h(x_1, x_2) & \cdots & \rho_h(x_1, x_n) \\ \rho_h(x_2, x_1) & & & \vdots \\ \vdots & & \ddots & \\ \rho_h(x_n, x_1) & \cdots & & \rho_h(x_n, x_n) \end{bmatrix}$$



- Spatial distribution is fully characterized by its mean and its covariance.
- Inverse-exponential correlation with $b=0.1L$, $0.5L$, and $1L$ is assumed.
- *Karhunen-Loève* expansion is used to create random fields.



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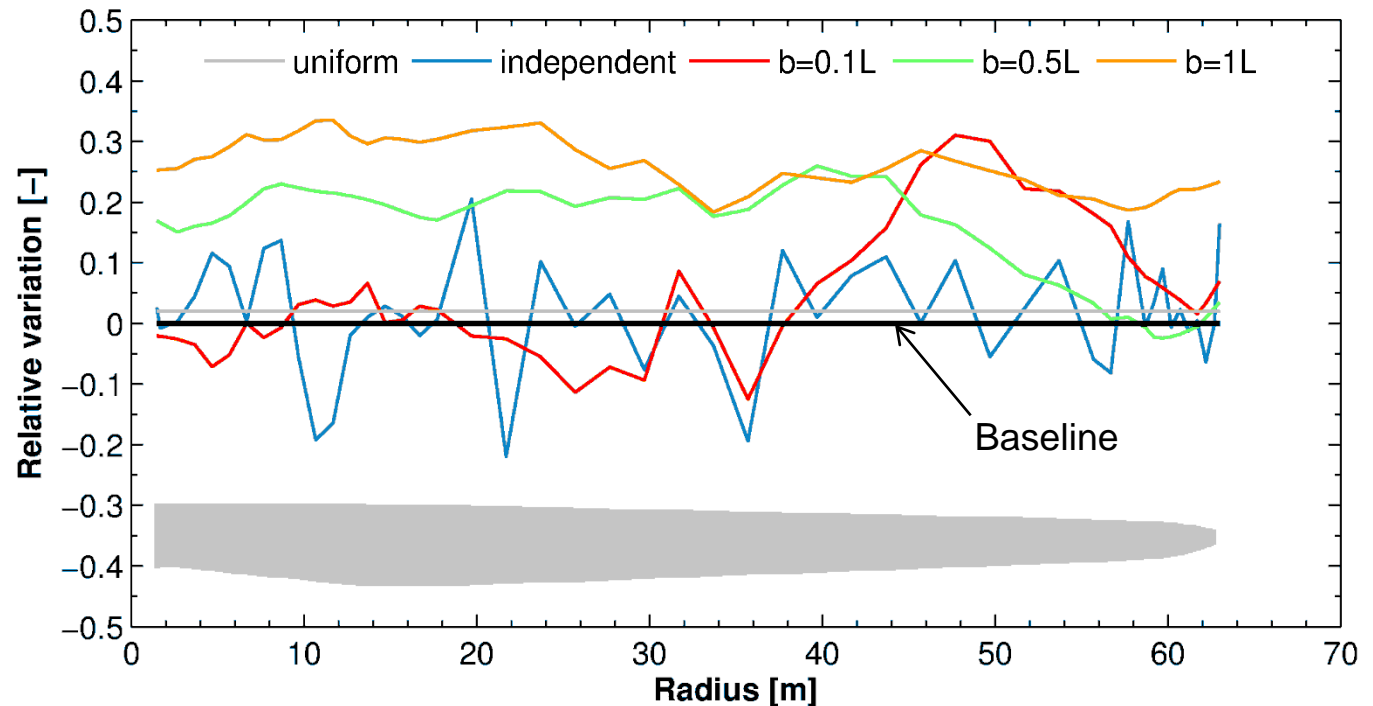
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Spatial Parameter Variations

The rotor blade is divided into 50 equally spaced elements/cross sections and 1000 samples are created for each type of spatial variation.



- Spatial independent variations can cause local extreme fluctuations.
- The correlation increases with an increasing correlation length b .
➔ Variations along the blade become smoother.



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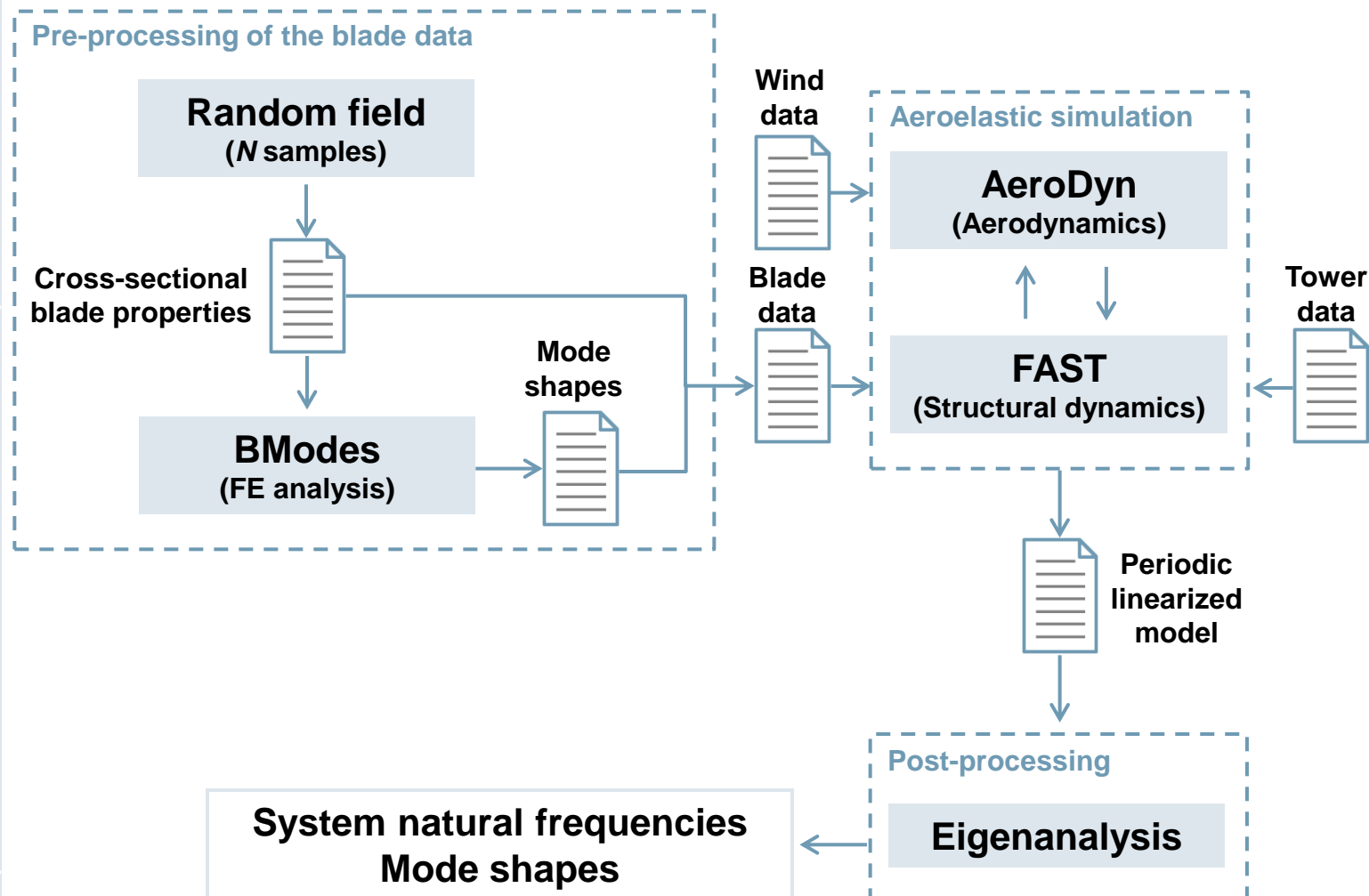
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FAST: Jonkman J. M. and Buhl Jr. M. J. (2005): *FAST User's Guide*. NREL/TP-500-38230. Golden, Colorado, USA: National Renewable Energy Laboratory

BModes: Bir G. S. (2005): *User's Guide to BModes (Software for Computing Rotating Beam Coupled Modes)*. NREL/TP-500-39133. Golden, Colorado, USA: National Renewable Energy Laboratory



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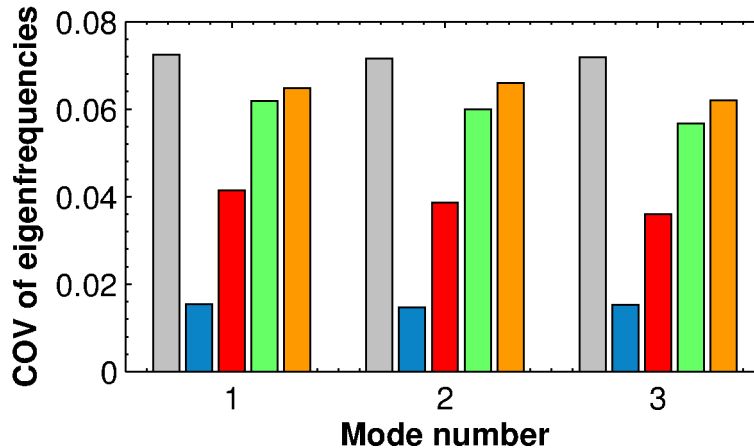
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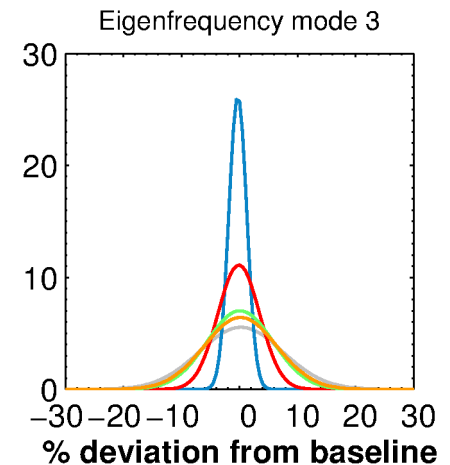
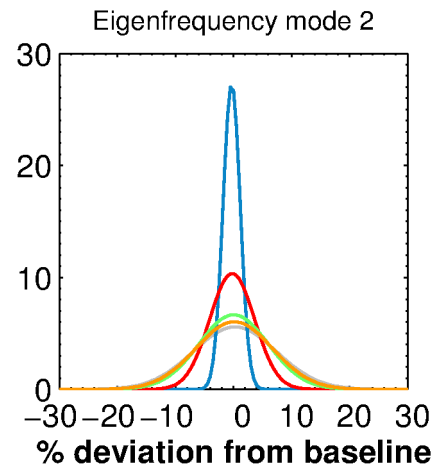
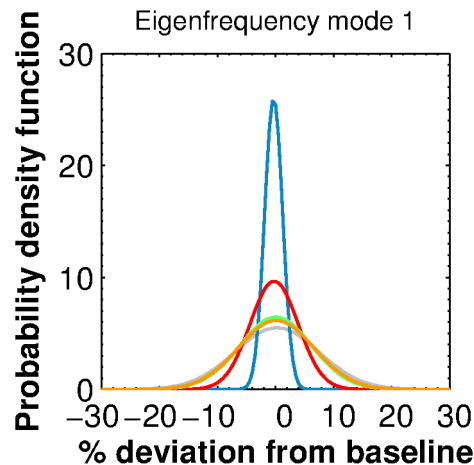
Conclusions and Outlook

Blade Eigenfrequencies at Standstill (BModes)



Coefficient of variation:

$$COV = \frac{\sigma_{\omega}}{\bar{\omega}}$$



— uniform — independent — b=0.1L — b=0.5L — b=1L

- ➔ Scatter of blade eigenfrequencies are almost identical
- ➔ Increase in scatter with increasing correlation length
- ➔ Relative deviations seem to be normally distributed

Variations of Blade Mode Shapes at Standstill (BModes)

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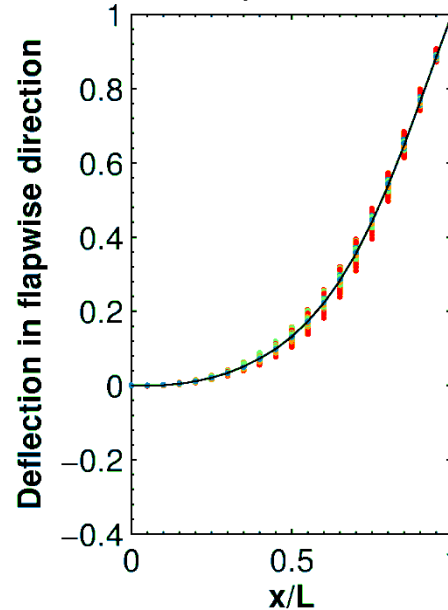
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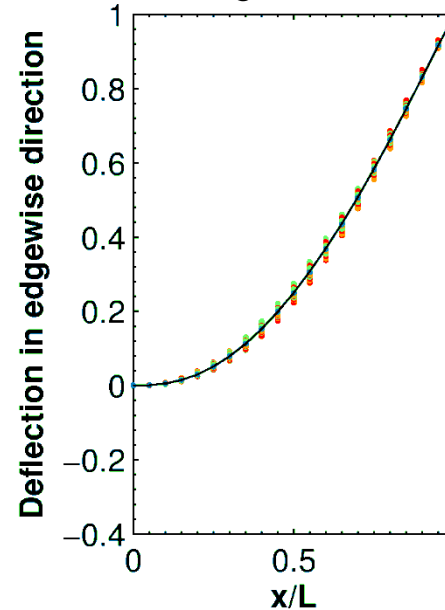
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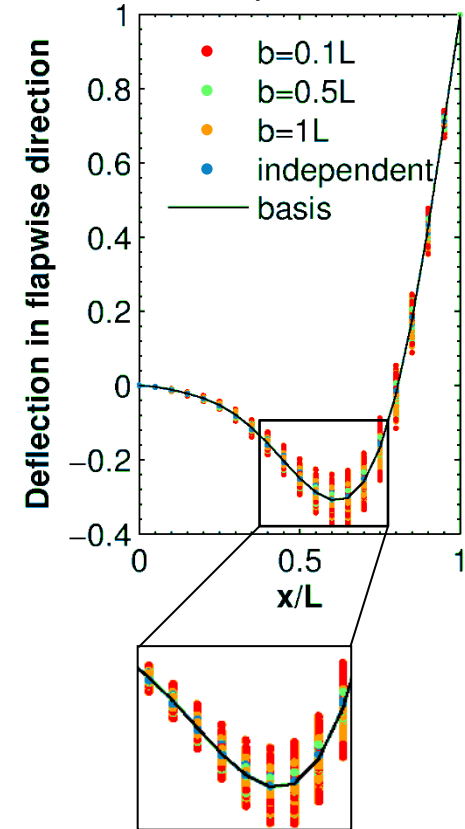
1st flapwise mode



1st edgewise mode



2nd flapwise mode



- ➔ No scatter of the mode shapes for spatially uniform variations
- ➔ Increase in scatter of the mode shapes with decreasing correlation length



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First 5 Rotor Modes at Standstill

The drivetrain and the tower-nacelle subsystem feel combined effects of all rotor blades.

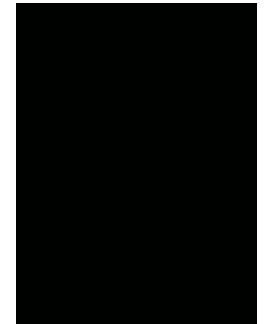
1st collective flapwise



1st flapwise yaw



1st flapwise pitch



1st edgewise yaw



1st edgewise pitch



Videos: standstill mode shapes of a 600 kW turbine (Hansen 2011)

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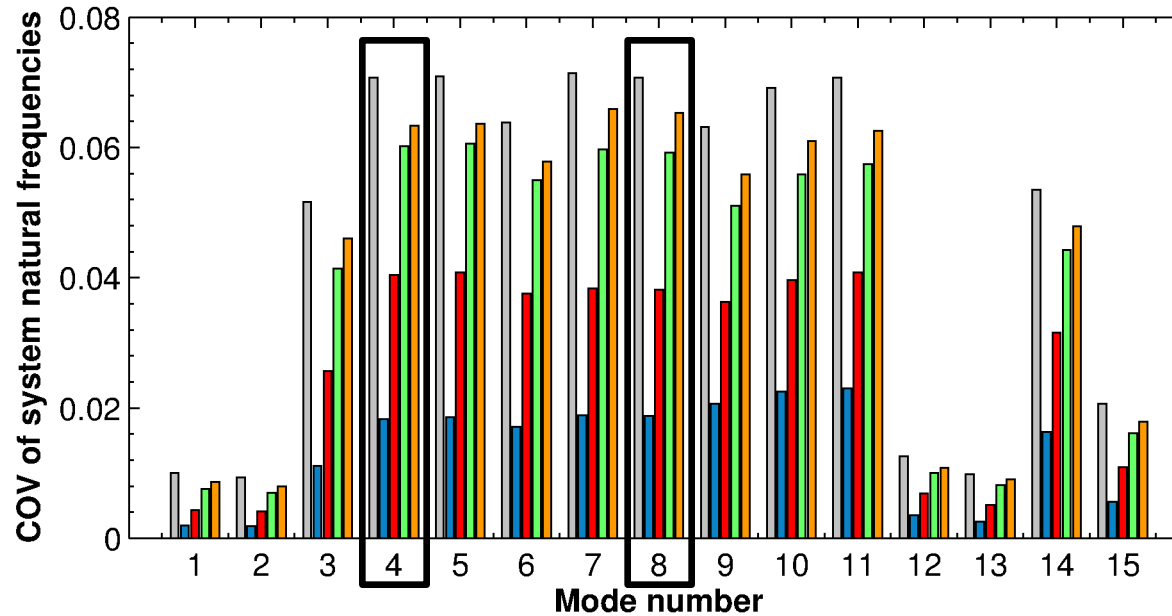
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System Natural Frequencies at Standstill (FAST)



Coefficient of
variation:

$$COV = \frac{\sigma_{\omega}}{\bar{\omega}}$$

1st tower bending
1st drivetrain torsion
1st flapwise bending
1st edgewise bending
2nd flapwise bending
2nd tower bending
1st edgewise bending
Nacelle yaw

- ➔ High frequency scatter for the rotor modes
- ➔ Significant impact on the drivetrain
- ➔ Almost no effect on the tower modes
- ➔ Correlation length $b=0.1L$ seems to be a reasonable assumption

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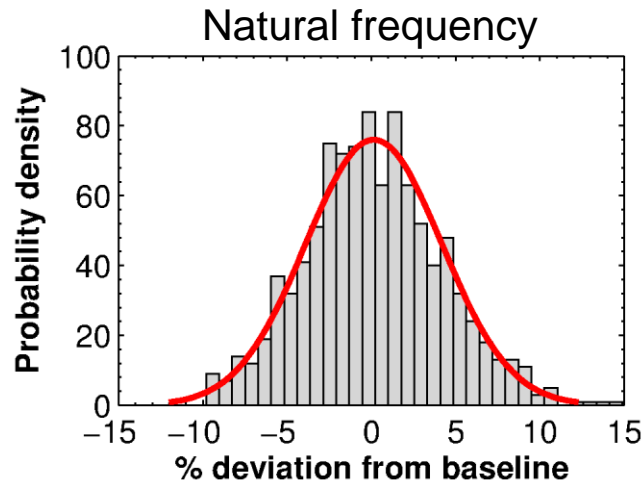
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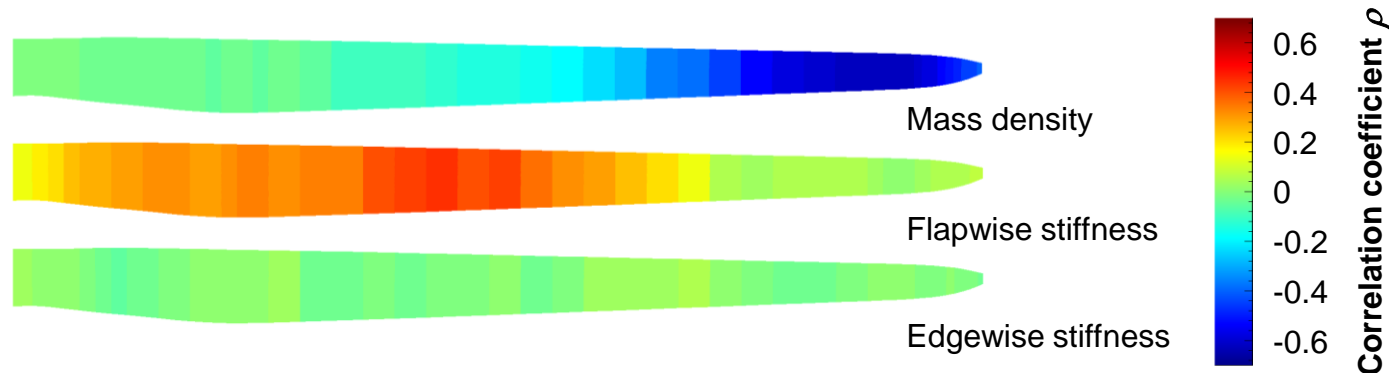
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Natural Frequency of the 1st Flapwise Yaw Mode ($b=0.1L$)



Hansen (2011)

Correlation between the structural parameters and the frequency



- ➔ Relative deviations follow a normal distribution
- ➔ Negative dependency between blade mass density and frequency
- ➔ Positive dependency between flapwise stiffness and frequency

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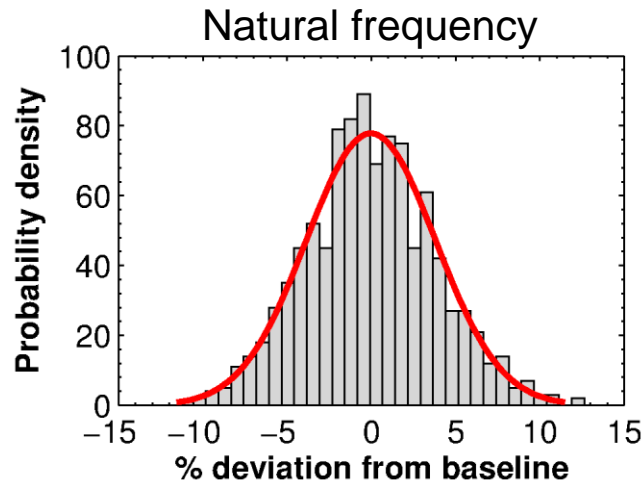
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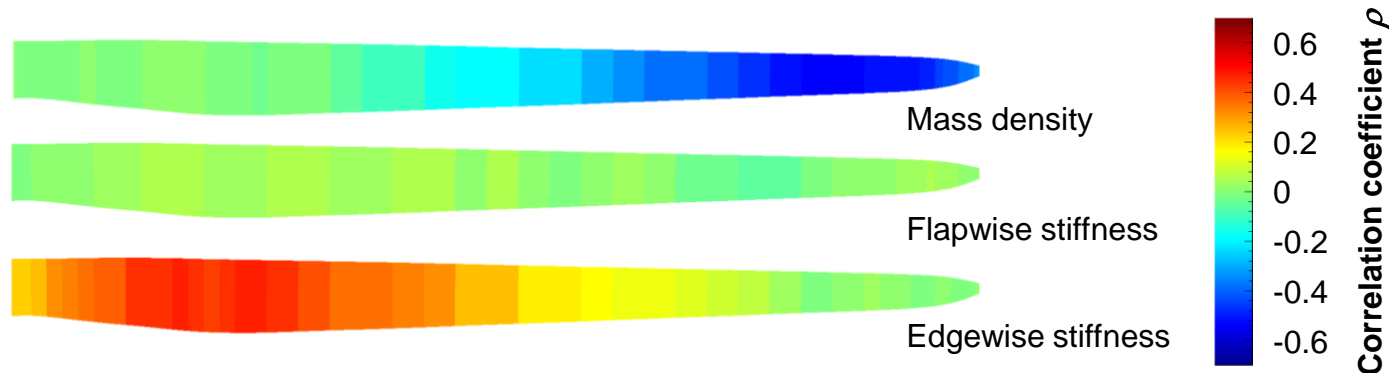
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Natural Frequency of the 1st Edgewise Yaw Mode ($b=0.1L$)



Hansen (2011)

Correlation between the structural parameters and the frequency



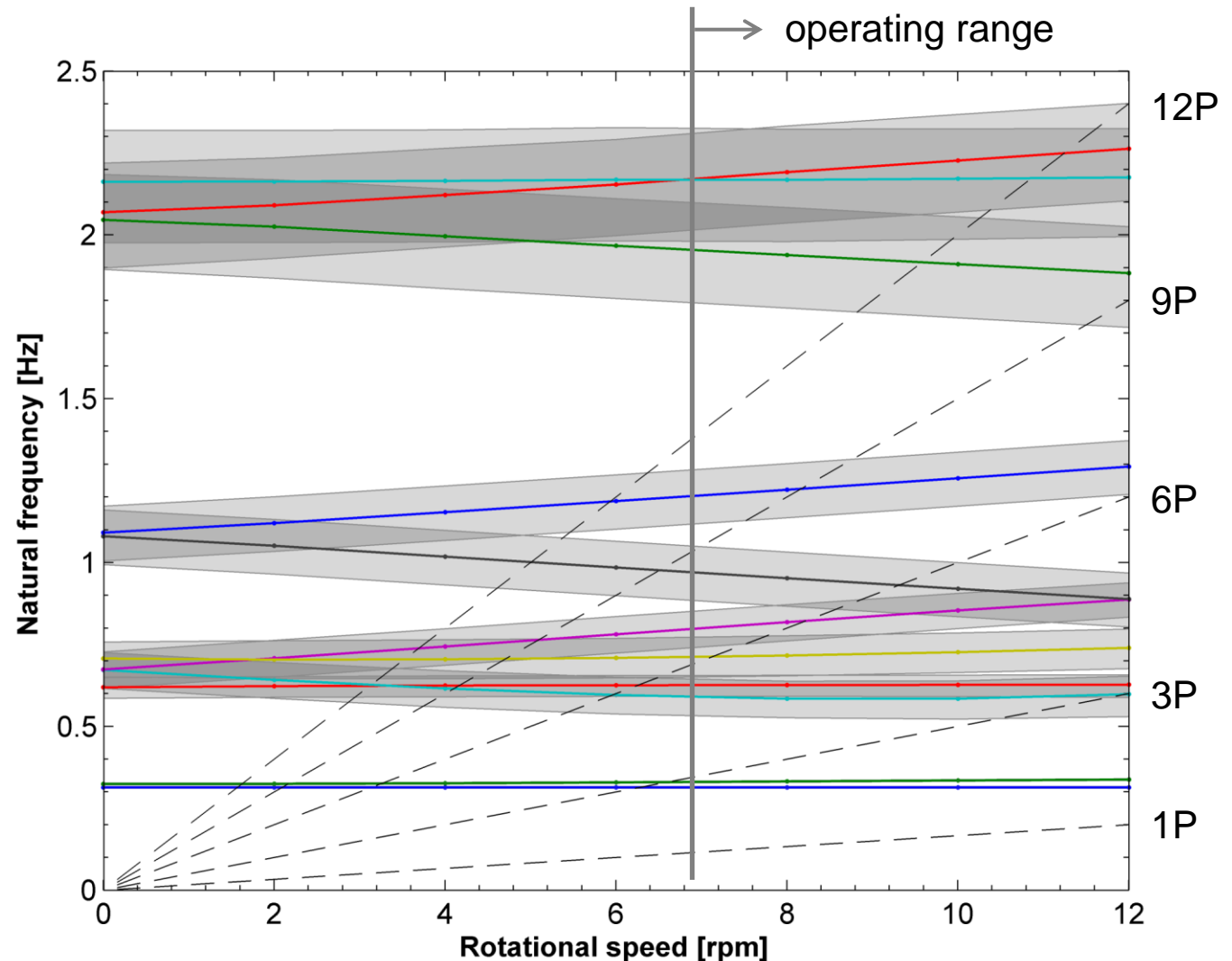
- ➔ Relative deviations follow a normal distribution
- ➔ Negative dependency between blade mass density and frequency
- ➔ Positive dependency between edgewise stiffness and frequency



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Campbell Diagram ($b=0.1L$)



- ➔ High frequency scatter of the rotor modes in the operating range
- ➔ Increased risk for resonances, e.g. drivetrain torsion and 3P frequency

Error bars: inter-quantile range $IQR=Q_{0.975}-Q_{0.025}$



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Conclusions

- Spatial uncertainty of structural blade parameters is modeled with a random field approach:
 - Increasing correlation length leads to a larger frequency scatter.
 - Correlation length $b=0.1L$ seems to be a reasonable assumption.
- Variations of blade structural parameters cause
 - a significant effect on blade eigenfrequencies and mode shapes.
 - a significant effect on system natural frequencies of the rotor modes.
 - an increased risk for resonances.
- Scatter of the frequencies follows a normal distribution.

Outlook

- Investigation of modal frequencies at different wind speeds
- Combined analysis of structural and geometric uncertainties
- Investigation of the effect on the loads

Thank you for your attention!

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